

MOULDS FOR THE PRODUCTION OF PLASTIC ABRASIVES AND

SUPPORT THEREOF

This invention relates to moulds for the production of plastic abrasives and their supports.

5 A mixture of thermosetting resins combined with abrasive powders, formed in suitable moulds by heat-curing in ovens, is used to make plastic abrasives.

In particular, the mixture of thermosetting resin and abrasive powder is poured into suitable moulds in the 10 liquid state and subsequently conveyed to ovens for heat-curing of the resin, this process being required to obtain the end product.

Plastic abrasives are usually manufactured in a continuous cycle, using automatic machines and tunnel 15 ovens.

The filling system will therefore be positioned at the entrance to the oven, while the system designed to eject the finished products from the moulds will be situated downstream of the heat-curing process, at 20 the outlet of the oven.

Heat-curing is one of the most critical stages in the process, because the properties of the end product depend on the way in which it is performed.

The uniformity of the material produced, and its 25 mechanical and physical characteristics, depend on

the efficacy of the curing process.

To obtain high-quality abrasives, it is necessary to use catalyses which give a high curing yield, with no limitations on the maximum exothermic temperatures of
5 the chemical reaction.

In this context, a known embodiment of moulds involves the use of thermoplastic materials such as polyethylene and polypropylene, or silicone rubber.

However, their use involves considerable drawbacks
10 associated with the chemical and mechanical aggressiveness exercised by the mixture on the moulds.

This chemical aggression is mainly due to the presence of styrene, a monomer contained in the
15 polyester resin, to the reaction by-products that form during the curing stage, and to the breakdown of the peroxide initiators.

The mechanical aggression is obviously due to the presence of abrasive fillers, mainly constituted by
20 quartz powders, in the mixture.

Moreover, the moulds undergo cyclical thermal stresses of heating and cooling due to their heating in the oven, and above all to the violent exothermic curing reaction.

25 As a result of these continual chemical, mechanical

and thermal stresses, the mould surface is subject to rapid deterioration with consequent pitting, to the point where it may be impossible to eject the finished products satisfactorily.

5 Moreover, if a production process with automatic machines working on a continuous cycle is used, inability to eject pieces due to mould deterioration problems will require all moulds to be replaced in advance.

10 This means that the moulds have to be replaced after a small number of manufacturing cycles, generating very large amounts of scrap. The average lifetime of the moulds used in applications according to the known art can be estimated at around 5 working days

15 at 8 hours a day.

Further disadvantages associated with the use of materials according to the known art are that they present low heat conductivity and a low heat capacity. This leads to low thermal efficiency of the

20 manufacturing cycle and uneven heating, and therefore curing, of the material contained in it. In view of their low heat capacity, the moulds arrive at the entrance to the tunnel oven at ambient temperature, thus further reducing the efficiency of the heat

25 exchange.

A very important factor is the rather low maximum temperature to which conventional moulds can be subjected, ie. not more than about 90°C.

This factor drastically restricts the choice of 5 solutions associated with the process chemistry and the reactivity of the raw materials.

Penalisation of the heat exchange to trigger the curing reaction in the mixture usually results in lower productivity.

10 A very large number of internal laboratory tests and in-process tests led us to consider the use of two types of coating for metal moulds: metal coatings such as chrome-plating, or fluorinated polymer coatings such as perfluoroalkoxy (PFA), fluorinated 15 ethylene propylene (FEP) resins and polytetrafluoroethylene (PTFE).

The former guaranteed excellent mechanical and thermal resistance, but ejection of the finished products was difficult.

20 The latter had excellent non-stick properties which facilitated ejection, but their resistance to thermal and chemical/physical stresses was very limited.

The innovation involved combining the properties of the two best solutions we had selected and 25 eliminating their drawbacks.

This invention offers a mould manufacturing process which, due to the chemical/physical characteristics of the material used to make the moulds, considerably increases mould life, improves the quality of the 5 products made in them, and increases productivity.

The invention also includes a support for moulds designed to manufacture plastic abrasives.

The moulds containing the mixture, placed close to the entrance of the tunnel oven by the filling 10 system, are conveyed automatically into said oven by means of a track belt on which the moulds are positioned.

In this context, a type of support used, for example, in the case of polypropylene moulds, is typically 15 constituted by parallel aluminium guides running transversely to the direction of advance.

These aluminium guides are hooked directly to the wings of the chains that move the moulds during the manufacturing process. Bars holding 5 to 10 moulds 20 integral with one another, depending on the size of the moulds, are inserted into said guides.

In the support system described above, the variable of primary importance in order to dimension the system correctly, is the chain pitch.

25 This value is used to establish the distance between

one guide and the next, thus defining productivity on the basis of the geometrical optimisation of the arrangement of the moulds on the support.

A further factor which should be taken into due account in the manufacture of said supports is the need to have differentiated chain pitches, based on the size of the moulds to be fitted. Chains of different sizes, each involving the use of a suitable crown gear, must consequently be employed. If a long pitch is needed to make large pieces, small-link chains are normally used, so that the moulds can be fitted alternately on the guides.

The main drawback of said methods is that a single chain of standard dimensions suitable for all types of production cannot be used.

The purpose of this invention is to solve the above-mentioned problems by providing a more versatile support for moulds designed to make plastic abrasives.

A further purpose of the invention is to provide a support for moulds designed to make plastic abrasives which features simpler assembly and access to the moulds.

These purposes are achieved by the moulds for the production of plastic abrasives and their supports

described in the annexed claims, to which the reader is referred for the sake of brevity.

The invention will now be described in detail, by way of example but not of limitation, with reference to

5 the annexed drawings, wherein:

figure 1 shows a perspective view of a mould designed for the production of plastic abrasives, and the corresponding support, according to this invention.

The set of moulds for the production of plastic
10 abrasives and their supports, according to this invention, is indicated globally in a sample embodiment by reference number 10.

Assembly 10 is designed for use with large-link drive chains, as illustrated in fig. 1. Plates 11 are
15 attached to suitable anchorage wings. Counterplates 12 are anchored to said plates 11 with a steel pin and a cotter pin.

Mould support guides 13 are secured to counterplates 12. The pitch of guides 13 is formed by suitably
20 drilling counterplates 12, which are easily removed.

Holes 14 for this fixing are visible. Guides 13 are preferably dovetailed.

Moulds for plastic abrasives 15 according to this invention are secured to guides 13 individually, by
25 means of a thread on the head which engages with a

perforated, threaded bar 16, which said bar is inserted into the corresponding guide 13.

Guides 13 and bars 16 are preferably made of aluminium.

5 The fixing system described has the further advantage of making individual replacements for maintenance purposes more versatile (by contrast with the known art, which uses bars with rows of integral moulds).

A particular heat-resistant material, which does not 10 dilate and is non-stick, was used to protect aluminium guides 13, namely teflon-impregnated fibreglass, which constitutes the protective tape.

Said tapes 17, containing holes 18 for moulds 15, are positioned between moulds 15, one of which is shown 15 in fig. 1 by way of example, and guides 13.

It is very important to note that the invention involves the use of metal moulds 15, coated with metal-matrix materials into which micronised teflon is mixed.

20 Alternatively, other substances with similar non-stick properties could be used.

This coating is preferably applied by means of non-galvanic treatments (chemical deposition).

The minimum thickness of said coating is the 25 thickness obtained by means of non-galvanic

treatments or chemical depositions for coating surfaces in general, and may be as little as a few microns.

In particular, in a preferred embodiment of this 5 invention, the minimum coating thickness with metal-matrix materials, with which at least one substance with non-stick properties is mixed in micronised form, is ≥ 10 microns.

Thus the advantages of both materials are exploited 10 and their disadvantages cancelled out, giving rise to numerous major advantages compared with the prior art.

Firstly, the high thermal conductivity of the material from which the mould is made increases the 15 productivity of the process and the quality of the end product, due to a better uniformity of heating.

Secondly, its excellent heat resistance, a value which influences the maximum operating temperature of the moulds (around 300°C), enables the oven 20 temperature to be increased, which leads to increased productivity.

Moreover, catalyses with high exothermic peaks can be performed, allowing the manufacture of products with a higher curing rate, leading to better quality.

25 Another significant variable in the plastic abrasives

production process is the mould temperature on entrance to the oven.

In processes performed by the prior art, the moulds reach the oven entrance at room temperature as they 5 do not possess the thermal capacity needed to stored the heat accumulated during the time spent in the oven.

The high heat capacity of the material used for the process according to the invention allows mould 10 temperatures of approx. 50-60°C, considerably increasing the productivity of the process.

Moreover, perfect coupling between the mixture and mould is achieved as a result of this property, because at the filling stage, the viscosity of the 15 mixture immediately declines near the area in which it comes into contact with the mould walls.

Further advantages of the subject of this invention derive from the fact that the material used to make the moulds possesses greater chemical resistance than 20 the materials conventionally used.

The result of this characteristic is a considerable increase in the time taken for the moulds to deteriorate, thus facilitating ejection of the pieces manufactured and increasing the productivity of the 25 process.

Moreover, the non-stick properties of the material that forms the mould coating facilitate ejection of the finished products.

As these moulds are not liable to deteriorate, the
5 presence of "spent" moulds, ie. rejects, is advantageously eliminated, thus eliminating the labour required to perform the lengthy operations of total prior replacement of the belts.

Finally, another significant advantage is that the
10 process produces plastic abrasives with perfect geometry, which is not affected by gradual, serious mould deterioration.

In particular "Metal matrix", one of the basic materials used in the coating of the mould according
15 to the invention, means one or more metals, or alloys thereof, selected from the group consisting of: nickel, copper, chromium, cobalt, manganese, titanium, iron, zinc, aluminium, rhodium, palladium, silver, platinum, gold, vanadium, tungsten, lead and
20 tin.

In a particularly preferred embodiment, the metal matrix is nickel.

"Substance with non-stick properties", the additional basic material used in the coating of the mould
25 according to the invention, means, in particular, one

or more fluoropolymers and, even more in particular, one or more fluoropolymers or mixtures thereof, selected from the group consisting of polytetrafluoroethylene (PTFE), fluorinated ethylene-
5 propylene resins (FEP), perfluoroalkoxy (PFA), polyvinylidene fluoride (PVDF), ethylene tetrafluoroethylene (ETFE) and ethylene chlorotrifluoroethylene (ECTFE).

In a particularly preferred embodiment of this
10 invention, the fluoropolymer is polytetrafluoroethylene (PTFE).

In a further preferred embodiment of this invention, the mould coating comprises a metal matrix in which at least one substance with non-stick properties,
15 preferably fluoropolymer(s), is mixed in micronised form in the percentage of 5% to 60% by weight, preferably 25% to 30% by weight, of the total weight of the metal matrix and the substance with non-stick properties.

20 In a further even more preferred embodiment of this invention, the mould coating consists of metal matrix in which at least one substance with non-stick properties, preferably fluoropolymer(s), is mixed in micronised form in the percentage of 5% to 60% by weight, preferably 25% to 30% by weight, the weight
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percentage of the metal matrix being its complement to 100%.

"Mixing in micronised form" of the substance with non-stick properties, such as the fluoropolymers 5 according to this invention in particular, means that said non-stick substance is mixed in the form of particles with an average size of 0.1 µm to 200 µm, in particular with a size of 0.5 µm to 100 µm, and more in particular in the form of particles with an 10 average size of 1 µm. In an even more preferred embodiment, the mould according to the invention is coated with materials consisting of a nickel metal matrix wherein polytetrafluoroethylene (PTFE) is mixed in the percentage of 25% to 30% in weight, the 15 percentage in weight of the metal matrix being its complement to 100%, and said PTFE in micronised form consisting of particles with an average size of 1 µm.

"Plastic abrasives manufacturing processes by baking mixtures consisting of thermosetting resins combined 20 with abrasive powders in ovens at high temperatures", conducted in coated moulds according to the present invention, means, in general, processes that involve baking in ovens of mixtures comprising thermosetting resins, such as urea-formaldehyde or polyester 25 resins, in the presence of heat initiators or

catalysts, such as peroxides or mineral acids, which said resins polymerise in the presence of abrasive powders or fillers such as quartz.

A further subject of this invention is therefore a
5 process for manufacturing plastic abrasive by baking
a mixture comprising at least a thermosetting resin
combined with an heat initiators or catalyst and an
abrasive powder or filler, wherein said mixture is
contained in a mould coated with metal-matrix
10 materials wherein at least one substance with non-
stick properties is mixed in micronised form.

The mould support to which this invention relates presents the following advantages compared with existing supports.

15 Firstly, the guide pitch is independent of the chain pitch.

This means that the drive chains are universal, and need not be replaced according to the size of the mould fitted.

20 Secondly, the belt configuration is changed simply by adjusting the counterplates to which the guides are attached, whereas in the solutions used by the known art, each guide must be removed and replaced individually.

25 A further considerable advantage of the use of chains

with large links is that they are more robust, thus considerably increasing the reliability of the entire system.

Finally, each mould is made so that it can be
5 attached individually, for example by screwing, to the perforated, threaded bar, which will be inserted into the guide.

This procedure advantageously increases the versatility of mould maintenance, assembly and
10 replacement operations.

The above description clearly demonstrates that the inventive concepts are not limited to the examples of application illustrated, but could also be advantageously adapted to other similar applications.

15 This invention is therefore liable to numerous modifications and variations, all of which fall within the scope of the inventive concept described in the annexed claims, while the technical details can vary as needed.

20 LABORATORY AND MANUFACTURING TESTS

Conical moulds with a base of approx. 20 mm in diameter were made with different types of materials, as follows:

- 1) Polypropylene moulds: type (a).
- 25 2) Moulds made of metal such as steel or aluminium:

type (b).

3) Moulds with metal coatings on a metal body, such as steel or aluminium with a chrome coating (the texture being gradually varied): type (c).

5 4) Moulds with fluoropolymer coatings (such as PFA, FEP and PTFE) on a metal body made of steel or aluminium; fluoropolymers declared to have high chemical and/or mechanical resistance: type (d).

10 5) Moulds with ceramic coatings on a metal body such as steel or aluminium: type (e).

6) Moulds made of PTFE with cavities cut out of the solid material: type (f).

15 7) Moulds with a metal body made of steel or aluminium, with a metal-matrix coating in which one or more fluoropolymers according to this invention are dispersed in micronised form, and with the specifications regarding the nature and composition of said coating reported in Table 1:

type (g).

20 Table 1

Metal matrix	Fluoropolymer	% weight of fluoropolymer	% weight of metal matrix	average size of fluoropolymer particles
Nickel	Polytetra-fluoroethylene (PTFE)	25-30	75-70	1 micron

The coating described in Table 1 is applied by non-galvanic (chemical nickel) deposition to the metal body of the mould.

In the case of coated moulds, said coatings of 5 different chemical natures all have the same thickness of 30 microns.

Plastic abrasives manufacturing processes have been conducted in moulds made with the specifications described above, under the same operating conditions, 10 by heat-curing mixtures comprising polyester resins with a peroxide catalyst in the presence of quartz powder in high-temperature ovens at the temperature of 110°C.

Parameters such as the following were evaluated at 15 the end of each process: the chemical and mechanical resistance of the mould, the ejectability of the finished piece from the mould, the number of manufacturing cycles before deterioration of the mould, and the overall conductivity of the mould, in 20 order to compare the various types of mould used under the same operating conditions. Said comparison is summarised in Table 2.

Table 2

Type of mould and material	chemical resistance	mechanical resistance	ejection of finished piece (non-stick properties)	no. of complete manufacturing cycles	total mould conductivity
Polypropylene mould: type (a)	acceptable	acceptable	only good when the mould is new	40	low
Metal mould: type (b)	excellent	excellent	poor	(ejection difficult)	good
Chrome-coated mould: type (c)	excellent	excellent	poor	(ejection difficult)	high
Metal mould with polymer coatings based on FEP, PFA or PTFE: type (d)	poor/good	poor to fair	excellent	from 2 (PTFE) to 150 (PFA)	high

Table 2 (cont..)

Type of mould and material	chemical resistance	mechanical resistance	ejection of finished piece (non-stick properties)	no. of complete manufacturing cycles	total mould conductivity
Mould with ceramic coating: type (e)	excellent	excellent	poor	(ejection difficult)	average
PTFE mould made from solid material: type (f)	excellent	barely acceptable	barely acceptable	90	very low
Mould with nickel/PTFE coating as described in Table 1: type (g)	excellent	excellent	excellent	>1000	high

As Table 2 clearly shows, the moulds to which this invention relates have properties of chemical and physical resistance and non-stick properties which are far superior to the simple combination of the 5 advantages of mechanical resistance originating from the metal component and the non-stick advantages of the fluoropolymer component, because the number of manufacturing cycles performed by the moulds according to the invention is at least one order of 10 magnitude greater than the maximum number of manufacturing cycles which can be obtained with moulds made with only one of the materials composing the coating layer of the mould according to the invention.